

A Study of the Far-infrared Optical Properties of Rexolite™

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As interest grows in optical and quasi-optical systems operating at terahertz frequencies, materials which may provide alternative solutions to the design of system components come under close scrutiny. In response to evaluating prospective materials for window and lens applications, the far-infrared optical properties of Rexolite™ 1422 were characterized at the University of Lowell Research Foundation (ULRF) using Fourier transform spectroscopy (FTS). The Rexolite™ used in this study was acquired from C-Lec Plastics, Inc. of Beverly, NJ and a sample was machined to a thickness of $t = 0.0236'' \pm 0.0002''$. Spectroscopic transmission measurements were performed on the sample over a wavelength region of 10 cm^{-1} to 360 cm^{-1} with a 0.1 cm^{-1} wave number resolution. See Figure 1.

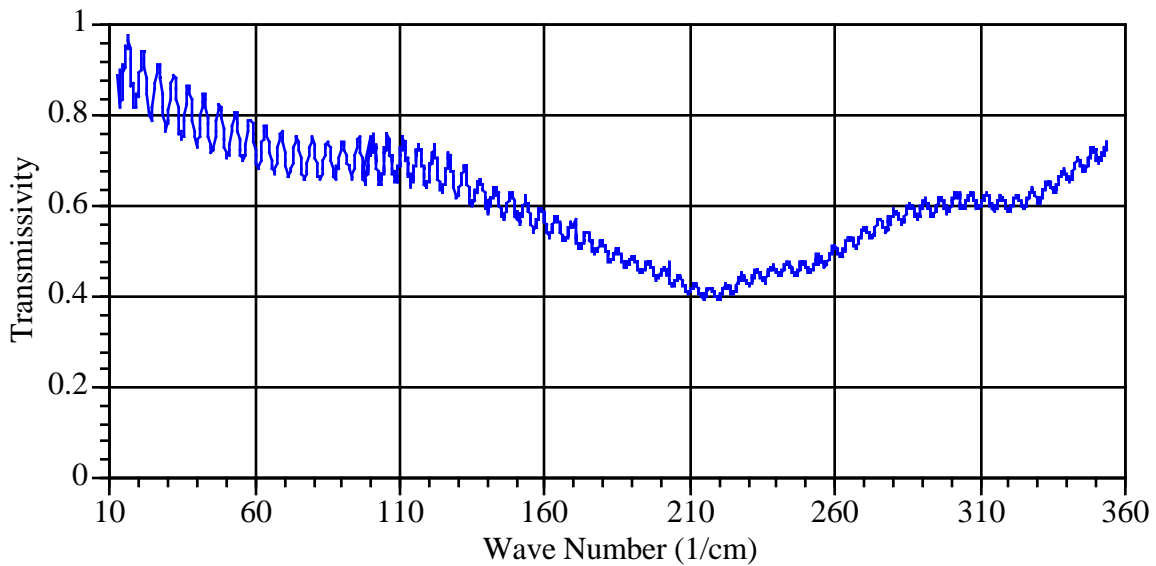


Figure 1. The FTS transmission data for a 0.0236" thick sample of Rexolite™.

The data's transmission peak location as a function of wave number was used to determine the material's refractive indices knowing the phase thickness()¹ relationship:

$$= 2 (N t /) \cos \theta_1 \quad \text{eqn. 1}$$

The internal refraction angle, θ_1 , is zero since the measurement was made at normal incidence. Each peak corresponds to a phase thickness of $= m$ where m is an integer. $N = n - ik$ is the complex refractive index where, during the determination procedure for n , the extinction coefficient, k , may be treated as negligible (i.e. $n \gg k$ for Rexolite™ in the far-infrared).

Measuring the wavelength at locations of two different transmission peaks allows calculation the refractive index using equation 1 in the following manner,

$$\lambda_2 - \lambda_1 = 2t \left\{ \frac{1}{\lambda_2} - \frac{1}{\lambda_1} \right\} n \quad \text{eqn. 2}$$

For example, Figure 1 allows evaluation of equation 2 over the measured wavelength region using values with a five peak separation. This calculation yields an average value of $n = 1.58 \pm 0.02$ for the refractive index. Uncertainty in these calculations stem from the interferometer's maximum resolution, 0.1 cm^{-1} , point to point location of the transmission peaks and the material's thickness tolerance ± 0.0002 ".

Table 1. The extinction coefficient for Rexolite™ as a function of wave number.

| 1/ (1/cm) | k | 1/ (1/cm) | k | 1/ (1/cm) | k |
|-----------|--------|-----------|--------|-----------|--------|
| 21.2 | 0.0028 | 132.4 | 0.0034 | 242.6 | 0.0038 |
| 26.2 | 0.0036 | 137.5 | 0.0036 | 248.2 | 0.0037 |
| 32.0 | 0.0043 | 142.6 | 0.0038 | 253.2 | 0.0034 |
| 37.0 | 0.0045 | 147.8 | 0.0039 | 259.1 | 0.0032 |
| 42.5 | 0.0047 | 152.9 | 0.0039 | 264.7 | 0.0029 |
| 47.8 | 0.0049 | 158.1 | 0.0040 | 270.3 | 0.0027 |
| 53.1 | 0.0049 | 163.5 | 0.0041 | 274.7 | 0.0025 |
| 58.4 | 0.0048 | 169.1 | 0.0041 | 279.7 | 0.0023 |
| 63.8 | 0.0049 | 173.5 | 0.0043 | 285.3 | 0.0021 |
| 68.9 | 0.0047 | 178.7 | 0.0044 | 290.4 | 0.0020 |
| 74.1 | 0.0047 | 184.6 | 0.0045 | 296.0 | 0.0020 |
| 79.7 | 0.0045 | 189.7 | 0.0046 | 301.8 | 0.0019 |
| 85.1 | 0.0044 | 194.9 | 0.0047 | 306.8 | 0.0019 |
| 90.3 | 0.0041 | 200.7 | 0.0047 | 312.0 | 0.0019 |
| 95.9 | 0.0037 | 205.6 | 0.0048 | 317.2 | 0.0018 |
| 100.0 | 0.0034 | 211.0 | 0.0050 | 322.8 | 0.0018 |
| 104.4 | 0.0032 | 216.5 | 0.0049 | 328.0 | 0.0017 |
| 111.0 | 0.0032 | 222.1 | 0.0048 | 333.0 | 0.0016 |
| 116.5 | 0.0032 | 227.2 | 0.0044 | 338.3 | 0.0014 |
| 122.1 | 0.0032 | 232.4 | 0.0041 | 343.5 | 0.0012 |
| 127.2 | 0.0033 | 237.5 | 0.0039 | 349.0 | 0.0010 |

With the refractive indices' real component (n) determined, calculations were performed to evaluate the far-infrared absorption of Rexolite™ using the Fresnel equations¹. The theoretical transmissivity which models the material's multiple reflection behavior:

$$T = \left| \frac{1 - r^2 e^{-i}}{1 - r^2 e^{-2i}} \right|^2 \quad \text{where} \quad r = \frac{N - 1}{N + 1}$$

was evaluated at 60 different frequencies across the submillimeter wavelength regime and matched to the measured data through adjustment of the extinction coefficient (k). The calculated values of $k \pm 0.0002$ are given in Table 1 and have been depicted graphically in Figure 2. While

precision of this analysis may not be adequate for all FIR design applications, the refractive index model generated can be used to determine the general optical behavior of FIR devices fabricated from Rexolite™ 1422.

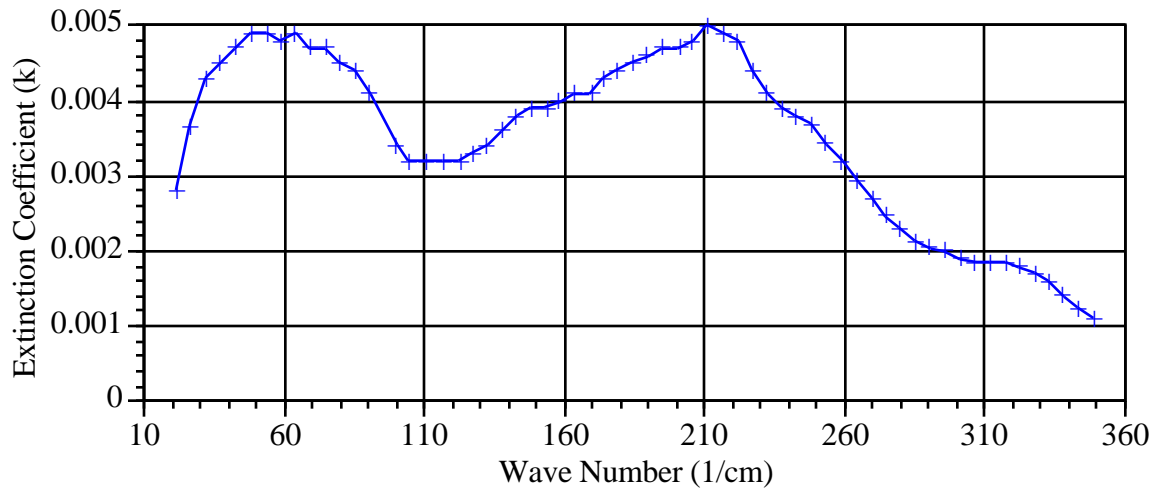


Figure 2. The extinction coefficient for Rexolite™ as a function of wave number.

References

1. R.M.A. Azzam and N.M. Bashara, Ellipsometry and Polarized Light, North-Holland 1979, Section 4.3